New Methods for Hydraulic Characterization of Mine Waste and Cover System Materials

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Overview

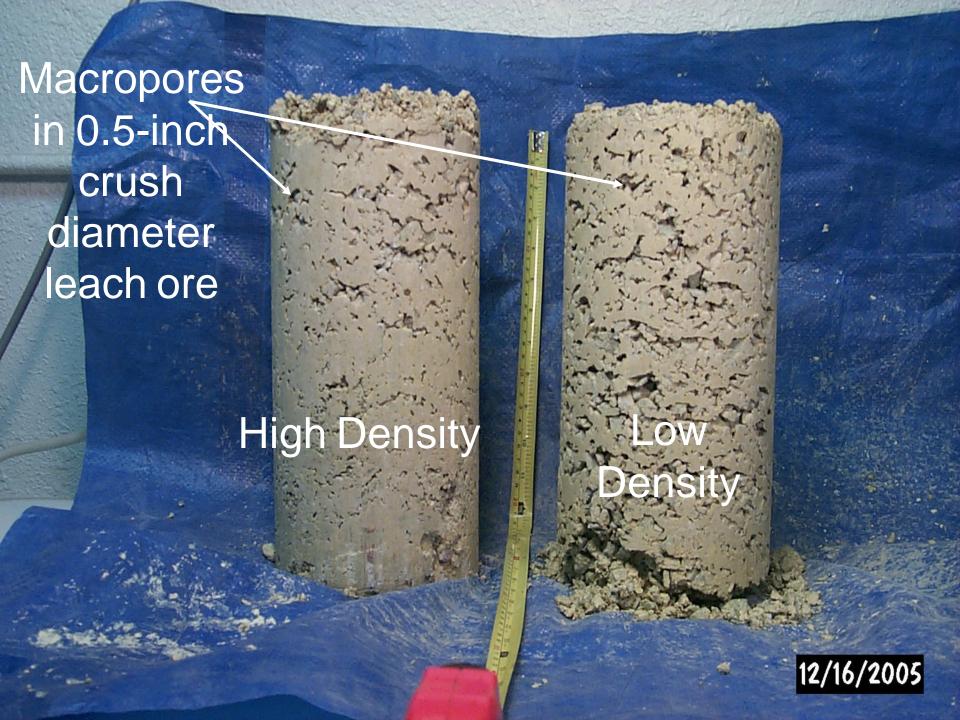
- Background review on hydraulic testing
- Review of new hydraulic tests
- Experiment with leach ore sample:
- Results
 - Data from 30 cm (12-inch) diameter core with new test methods vs 5 cm (2-inch) core traditional test method
 - Model predictions
 - HYDRUS 1D
 - MACRO 5.0 (includes macroporosity)



Background

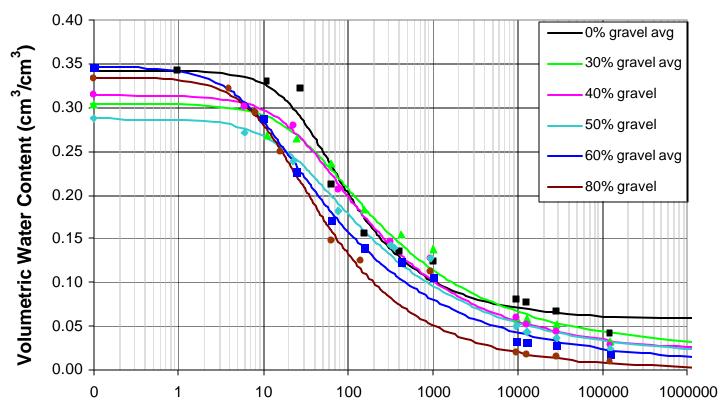
- Mine materials have lots of rocks......
- Presence of rock/gravel affects flow properties
 - Small amounts act as barriers to flow
 - Large amounts can create macropores = preferential flow
- Current laboratory methods were not designed for gravelly materials
 - Based on agricultural or well engineered soils
 - Remove rocks from sample, use correction factors
 - Theoretical assumptions for data analysis can be invalid
 - Macropore flow has been observed even in agricultural soils (>-4 cm)





Removing Gravel from Samples Can Give Very Different Results

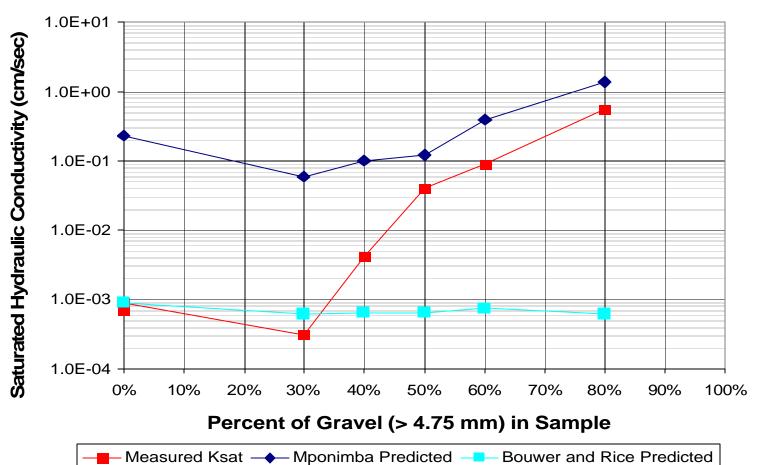
Moisture Retention Characteristic







Correction Factors?





Why is This Important?

- We build models to design for closure:
 - Estimate heap leach draindown
 - Estimate cover performance
 - Estimate water balances
- Consequences can be costly
 - Oversize/undersize water treatment
 - Excess infiltration/deep percolation
 - Underpredict water holding capacity of waste
 - Underpredict drainage response to storm events
- Need to develop cost-effective methods that will:
 - Be representative
 - Truly define Unsaturated flow characteristics



Obstacles

- Accurate soil water retention measurements in gravelly samples are difficult
 - Near saturation, moderate and dry tensions need different measurement methods
 - Big changes in flow with small changes in water content at wet range
 - Impossibly slow water movement in moderate tension to dry range (test could last for months to years)
- Cost and robustness
 - Large sample sizes needed for representativeness
 - Large columns (i.e. heap leach) columns are very expensive
 - Scaling of columns to larger systems

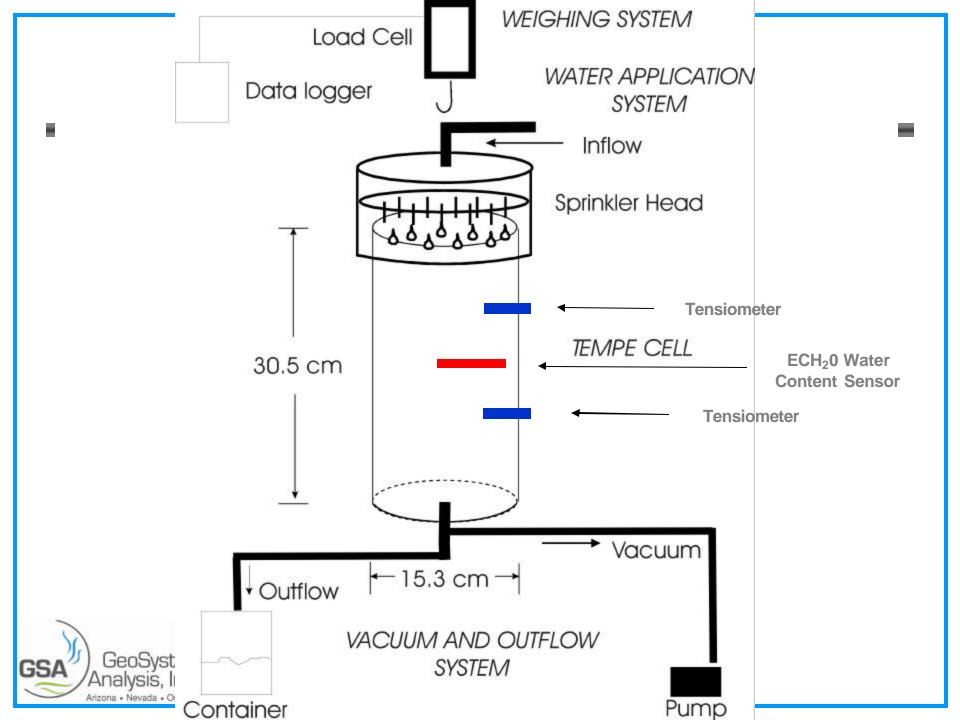


New Hydraulic Testing Methods

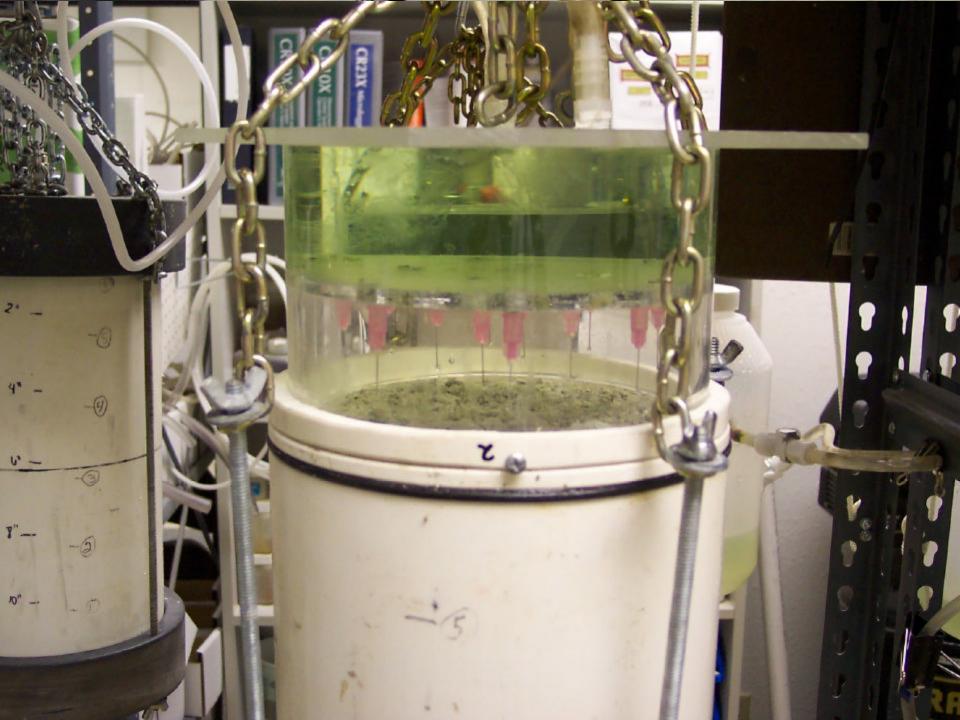
- 1. Review PSD data to determine the core diameter needed
 - Do not remove more than 20% of sample
 - 19 mm (0.75 inch) max particle diameter for 15 cm (6-inch) diameter core (8X)
 - 38 mm (1.5 inch) max particle diameter for 30 cm (12-inch) core (8X)
- 2. Pack and instrument large diameter cores with water content (ECH₂O) and tensiometer sensors
- 3. Conduct laboratory measurements for:
 - a. Unsaturated irrigation at 10⁻³, 10⁻⁴ and 10⁻⁵ cm/sec
 - b. Allow 3 to 5 day drainage periods between irrigation cycles
 - c. Saturated hydraulic conductivity
 - d. Measure soil water retention characteristics
 - i. Hanging column and Tempe cell for wet and moderate tensions
 - ii. Chilled mirror for dry points

New Hydraulic Testing Methods











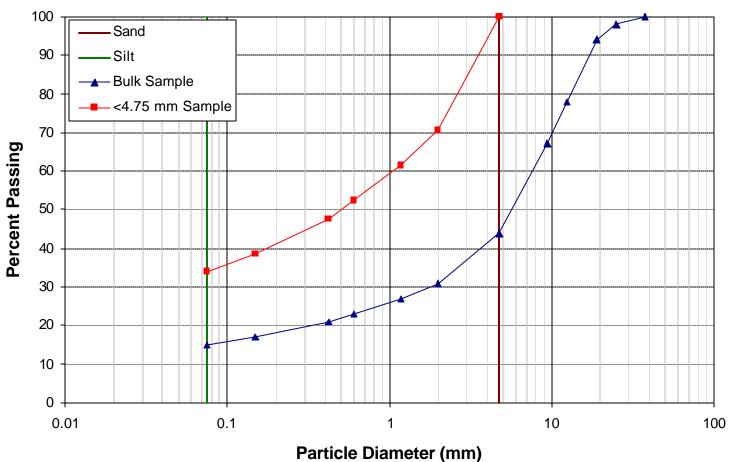
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Characterization Experiment





Sample Particle Size Distribution





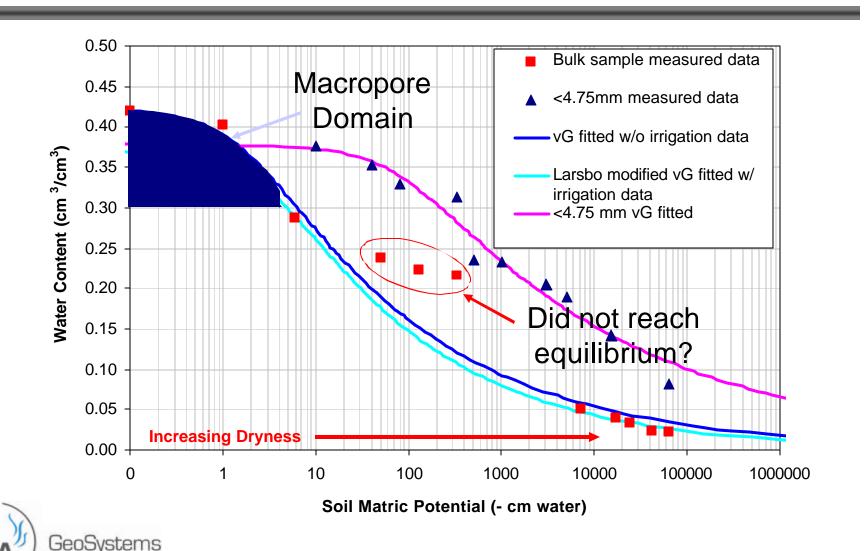
Experimental Design

- 12-inch diameter column, measure:
 - Saturated hydraulic conductivity
 - Water content and tension at known hydraulic conductivity (irrigation experiments)
 - Soil water retention characteristics (water content vs tension)
 - Chilled mirror for dry points
- Outside laboratory
 - Measure saturated hydraulic conductivity in 8-inch diameter cores
 - Soil water retention characteristics in 2-inch diameter cores (screen samples)
- Model results using:
 - HYDRUS-1D (van Genuchten)
 - MACRO 5.0 (Larsbo)
 - Assumes matrix flow follows van Genuchten
 - Macropore flow is kinematic wave
 - Define macropores as region between saturation and -4 cm

Experimental Results

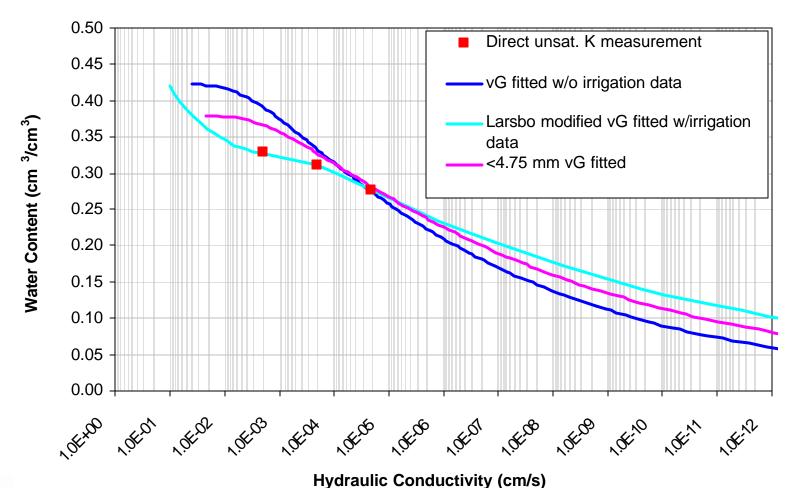


Soil Water Retention Characteristics



Analysis, Inc.

Hydraulic Conductivity

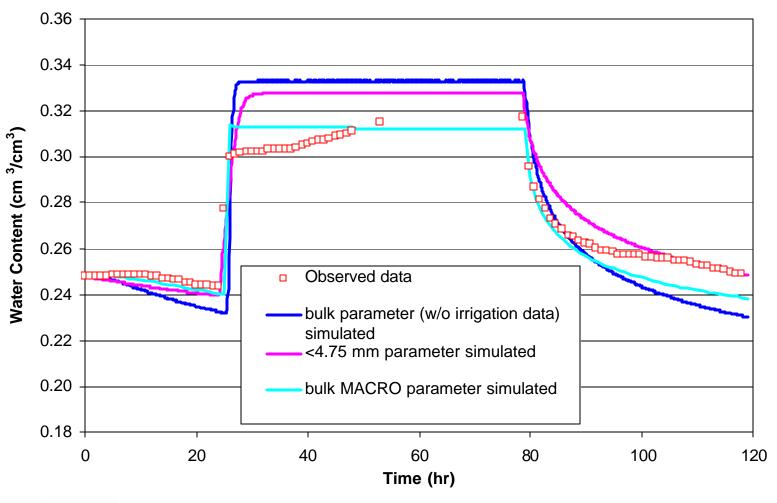




Modeled Results



Simulated Water Content

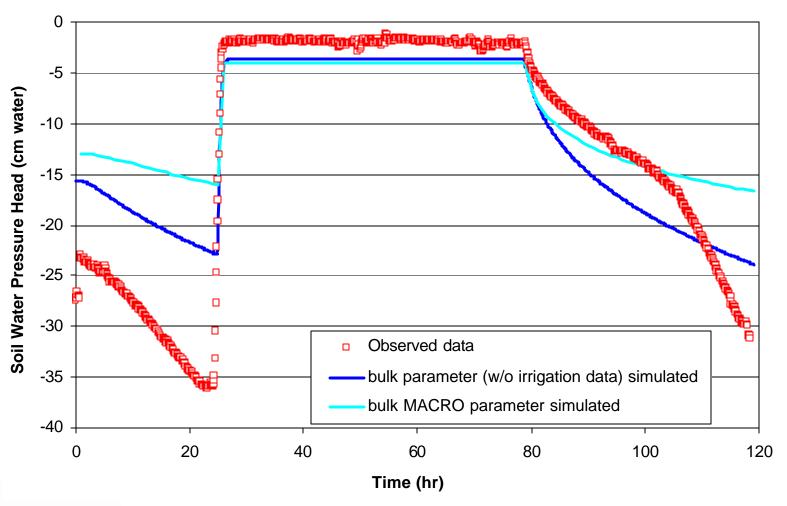




Is the 2-inch Core Data Really That Good?

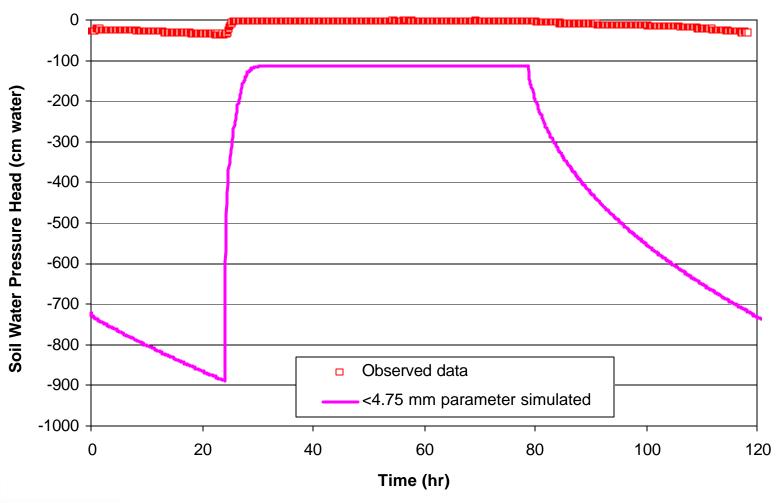


Bulk Parameter Simulated Pressure Head





< 4.75 mm Parameter Simulated Pressure Head





Dual Wall Ksat and Kunsat

- The purpose of developing the dual wall testing device and protocols are:
 - To minimize the edge effect between test material and rigid wall
 - To enable different tests in one flow cell, thus less samples needed
 - To avoid vertical differential compaction
 - To reach more uniform compaction



Ore 1

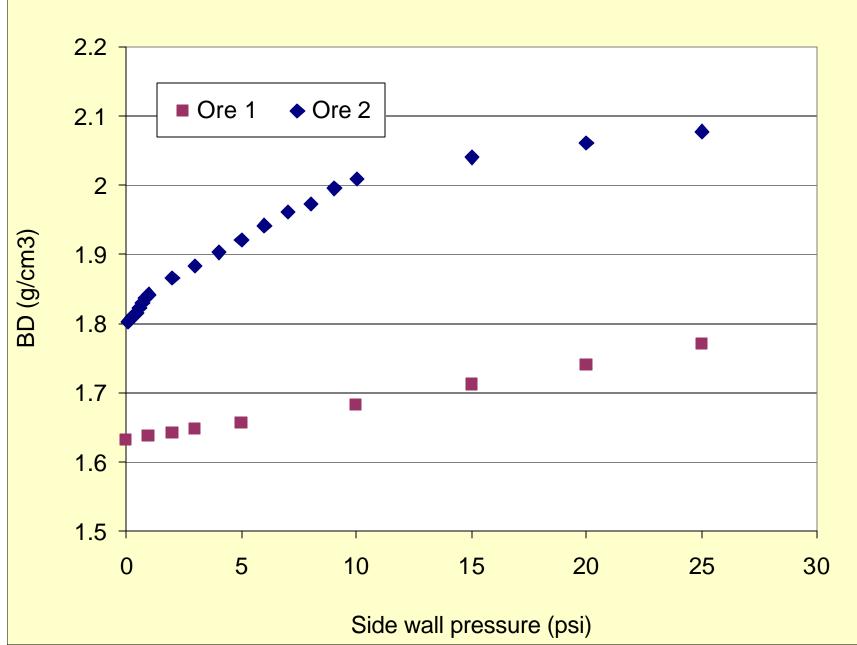


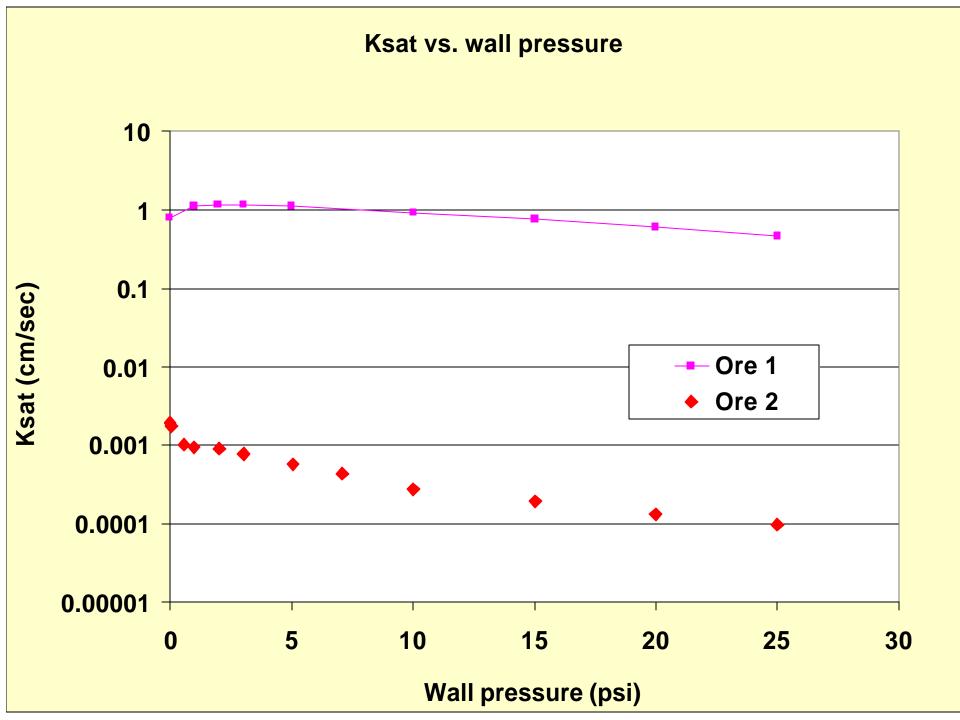
Ore 2





Dual wall BD-side wall pressure





Conclusions

- New laboratory methods appear to:
 - Significantly improve our ability to forward model
 - Question our ability to measure soil water retention characteristics for gravelly material at moderate and dry tensions
 - Question whether currently accepted laboratory methods can be used to model gravelly systems
- Removing gravel and determining MRC on 2-inch cores:
 - Does not scale to larger sample sizes
 - Can lead to gross errors in modeling
- Need to account for effect of macropore flow
- More research needed to:
 - Confirm new laboratory methods
 - Define when matrix flow ends and macropore begins?
 - Measure unsaturated flow rates at moderate tensions
 - Model macropore systems



